

# WAVEFORM DISTORTIONS DUE TO AC/DC CONVERTERS FEEDING DC ARC FURNACES

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*Abstract* – **The line-commutated converters are cause of significant harmonic distortions in electrical power systems. They can operate as a six-pulse converter or configured in parallel arrangement for high-pulse operation; twelve-pulse converters are usually used for DC arc furnaces. The DC arc furnaces can cause time-varying power quality disturbances in the feeding network, mainly waveform distortion and voltage fluctuations. In this paper the problem of the waveform distortion assessment of these important disturbing loads is taken into account. The study is performed using computer simulation based on Power System Blockset, that is a tool of Matlab, and using a chaos-based model for simulating the dc arc.**

## 1. INTRODUCTION

AC and DC arc furnaces represent one of the most intensive disturbing loads in the sub-transmission or transmission electric power systems; they are characterized by rapid changes in absorbed powers that occur especially in the initial stage of melting, during which the critical condition of a broken arc may become a short circuit or an open circuit.

In the particular case of the DC arc furnaces, the presence of the AC/DC static converters and the random motion of the electric arc, whose non-linear and time-varying nature is well known, are responsible for dangerous perturbations such as waveform distortions and voltage fluctuations. The converters are current controlled in order to limit current fluctuations in the electrodes.

While several papers in the relevant literature analyse the problem of the waveform distortion assessment in three-phase line-commutated current-controlled converters used in AC and DC motor drives and in HVDC links [1, 2], only few papers analyse the converters behaviour in DC arc furnaces. Recently in [3] this problem has been considered with the aim to outline the interactions between the converter control system and the waveform distortions and voltage fluctuations; the dc arc is simulated with a non-linear resistance whose values have been determined on the basis of measurements of the dc arc voltage.

The aim of this paper is to analyse both the waveform distortions caused by the DC arc furnaces on the feeding network and of the effects caused by the feeding network distortions and unbalances on the AC/DC static converter behaviour. In particular, this analysis uses a chaos-based model to represent the dc arc behaviour; in fact, the chaos theory, i.e. the Chua Circuit, has proven to be a very accurate and suitable model for assessing waveform distortions [4]. Moreover, in order to better evidence the time-varying nature of the waveform spectral components, Short Time Fourier Transform and high-resolution methods are applied [5, 6]. Particular attention is paid to outline the interactions between the supply voltage quality and the behaviour of the AC/DC converter control system.

## 2. DC ARC FURNACE IN STUDY

The typical dc arc furnace plant shown in Fig. 1 is considered as test system in this paper. It consists of a dc arc connected to a medium voltage

AC busbar with two parallel thyristor rectifiers that are fed by transformer secondary winding with  $\Delta$  and Y connection, respectively. The AC/DC converters are controlled with a DC current control system.

The medium voltage busbar is connected to the high voltage busbar with a HV/MV transformer whose windings are Y- $\Delta$  connected.

The system shown in Fig. 1 has the following parameters [4]:

**PCC**

Rated voltage: 220 kV

**Transformer T<sub>1</sub>**

Rated power: 80 MVA

Rated voltage: 220kV/21kV

V<sub>cc</sub> 8%

Winding connection: Y- $\Delta$ .

**Transformer T<sub>2</sub>**

Rated power: 87 MVA

Rated voltage: 21kV/0,638kV/0,638kV

V<sub>cc</sub> 10,37%

Winding connection:  $\Delta$ - $\Delta$ -Y

Interphase reactor: 150  $\mu$ H

Arc furnace rated current: 96 kA.

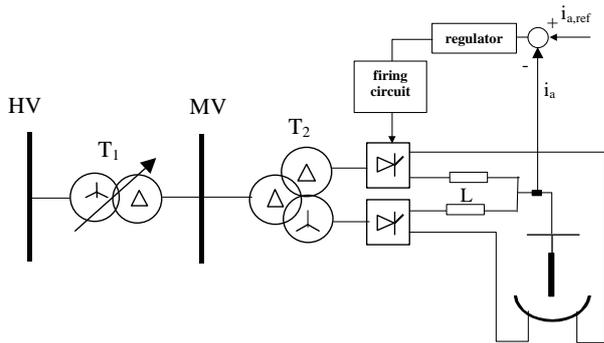


Fig. 1 - Dc arc furnace plant

In the dc arc furnaces the presence of the ac/dc static converter and the random motion of the electric arc, whose non linear and time-varying nature is known, are responsible for dangerous perturbations, in particular waveform distortions and voltage fluctuations; these perturbations are time-varying. In order to better evidence the waveform distortion problems, neither filters nor reactive compensation devices are initially provided.

**3. DC ARC FURNACE MODEL**

In this paper, the simulation of the DC arc furnace.plant has been developed by means of Power System Blockset, that is a tool of Matlab.

A chaos-based model for the dc arc furnace has been used.

In fact, in [4] it has been shown that the DC arc voltage waveform has the irregular behaviour that characterizes every chaotic phenomenon. This has been demonstrated with the analysis of proper delay plots and the evaluation of the largest Lyapunov exponent.

Some chaos based models have been analysed (Rossler, Chua and Lorenz models) in literature; in this paper, the Chua model has been employed due to its usefulness for waveform distortion forecasting.

The Chua model is based on the following equations:

$$\dot{x} = \begin{cases} \alpha(y - b_2x - (b_2 - a_2)), & \text{if } x < -1 \\ \alpha(y - a_2x), & \text{if } -1 \leq x \leq 1 \\ \alpha(y - b_2x - (a_2 - b_2)), & \text{if } x > 1 \end{cases}$$

$$\dot{y} = x - y + z$$

$$\dot{z} = -\beta y \tag{1}$$

In (1) x, y and z are the state variables and a<sub>2</sub>, b<sub>2</sub>,  $\alpha$  and  $\beta$  the model parameters, whose values have to be set as the most suitable for dc arc simulation. In particular, in this paper the optimal procedure proposed in [4] to set the parameters of the arc model has been applied.

With reference to the AC/DC converter control system, a DC current control system is usually employed. It clearly influences the time variations of the AC side current and voltage waveforms spectral content.

The current control system can be composed by a DC current control loop and a phase lock-loop (PLL) [3].

The DC current control loop acts such that, firstly, the actual output current of the converter is smoothed by a first-order time-delay element. Then, the filtered values are compared with the reference current. The so obtained error is the input of a PI controller that allows the evaluation of the delay control angle for the thyristors.

The PLL provides the reference system for the thyristor control angles of the converters. For this purpose the actual bus voltages are transformed in orthogonal components to evaluate the phase angle which is, in turn, compared with the control variable. The resulting deviation is smoothed and is the input of a PI controller. After comparison with the power system frequency, the control variable (phase angle) is generated by an integrator.

In [3] each of the DC arc furnace converters is provided of a separate current control system.

As an alternative, the reference angle for the thyristor control of the converters can be obtained by filtering the supply three-phase voltage

waveforms. Moreover, both AC/DC converters can be controlled with only one current control system.

#### 4. SOME CONSIDERATIONS ON DC ARC FURNACE WAVEFORM DISTORTIONS

The analysis of the current and voltage waveforms on the AC side of a DC arc furnace reveals an aperiodic behaviour, in spite of the converter dc current control. This is due to the strong non-linear and time-varying nature of the dc arc.

From a theoretical point of view, an aperiodic behavior could involve voltage and current spectral components (harmonics and interharmonics) that can be time-varying both in amplitude and frequency.

In the particular case of the numerical simulation of the DC arc furnaces, harmonics with time varying amplitudes can be forecasted due to the presence of the AC/DC converters and interharmonics can arise according to the DC arc model and behaviour.

As well known, a method for studying waveform distortion indices for time-varying signals in power systems is the short-time Fourier transform (STFT) where the Fourier transform is applied to a windowed signal [7].

The main problem in applying the STFT is the choice of the window length, having in mind that this choice constraints also the frequency resolution.

In particular, the choice of a short time window can cause the presence of unexpected spectral components, for instance uncharacteristic harmonics or a direct component, as shown in Fig. 2 a) where a 20 ms time window has been used; moreover, it can exalt the desynchronisation effects, mainly in presence of measurements on actual plants<sup>1</sup>. On the other hand, the choice of a too large window can generate averaged harmonics and a wide range of interharmonics, as shown in Fig. 2 b), where a 1 s time window has been used.

To better evidence the aforementioned problems with an other example, in Figs. 3 a) and b) the amplitudes of the voltage spectral components at the frequencies closest to 50 (fundamental) and 550 Hz (11<sup>th</sup> harmonic order) have been plotted versus the time window length (in the next these components will be named as

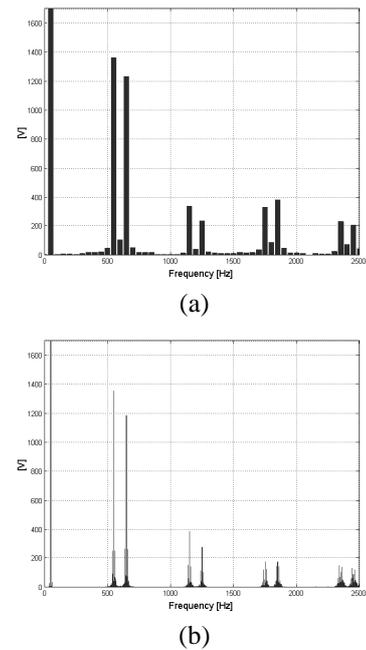


Fig. 2 - FFT spectra: a) 20 ms window; b) 1 s window

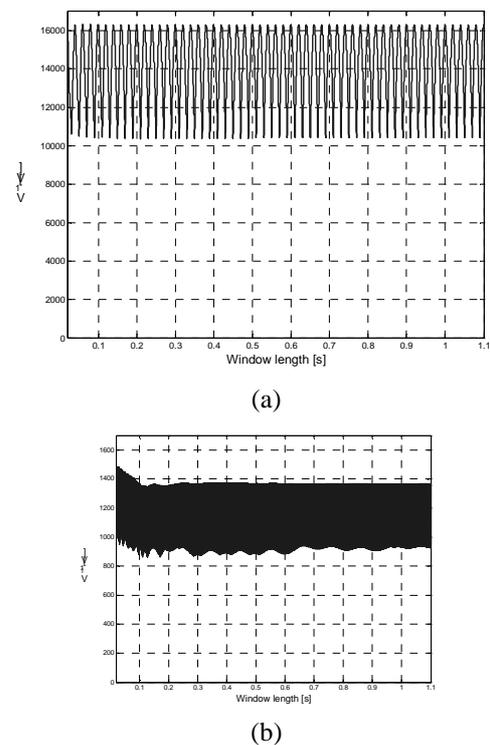


Fig. 3 - Amplitudes of the spectral components  $\tilde{V}^1$  (a) and  $\tilde{V}^{11}$  (b) versus time window duration

$\tilde{V}^1$ ,  $\tilde{V}^{11}$ )<sup>2</sup>; Figs. 4 a) and b) show a zoom of Figs. 2 a) and b), respectively, around 1 s.

<sup>1</sup> It is well known that the amount of interactions between different spectral components reduces increasing the time window.

<sup>2</sup> It should be noted that when a continuous time window is taken into account, the frequency resolution changes accordingly, with the consequence that, for some time windows, the 50 and 550 Hz components can disappear while spectral components close to them appear.

As it clearly appears from the analysis of Figs. 3 and 4, the maximum values of both  $\tilde{V}^1$  and  $\tilde{V}^{11}$  appear when the synchronisation condition is verified ( $T_{w(n)}$  and  $T_{w(n+1)}$  in Figs. 4, being these time

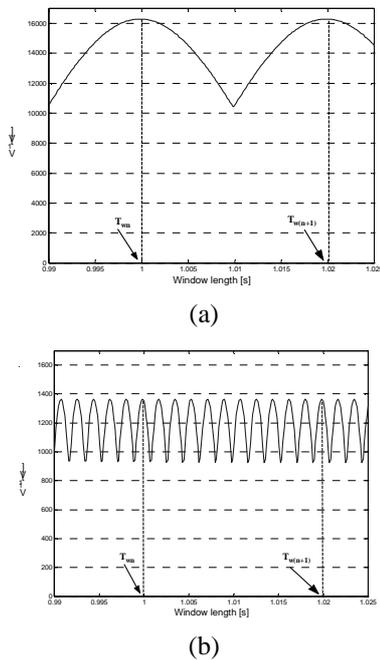


Fig. 4 - Zoom of the amplitudes of the spectral components  $\tilde{V}^1$  (a) and  $\tilde{V}^{11}$  (b) in Fig. 3

durations integer multiple of the fundamental period  $T_f = 20$  ms); these amplitude values are decreasing versus time (Figs. 3).

It is interesting to note also that the maximum values repeat with a constant period, as clearly evidenced in Figs 4, so confirming the constant frequency behaviour versus time of the examined components.

Similar considerations can be effected with reference to other harmonics.

Having in mind the aforementioned problems, in the next some considerations about the waveform distortion behaviour of the DC arc furnace plant in Fig. 1 will be effected referring to the indications of the IEC Std 61000-4-7, that is by using an FFT with a 10 AC cycle rectangular window and considering the subgrouping procedure.

First of all, the harmonic and interharmonic subgroup amplitudes have been calculated in order to compare the waveform distortion behaviour with different control systems. In fact, as clearly shown in [3], the waveform distortions on the AC side are influenced by the converter control system behaviour; a wrong choice of the control system parameters can determine unreasonable results.

The following cases have been considered:

1. the current control system is composed by a DC current control loop and a PLL with each converter provided of a separate current control system (Fig. 5);
2. as in 1. but with both AC/DC converters controlled with only one current control system (Fig. 6);
3. as in 1. but with incorrect values for the control system parameters (Fig.7).

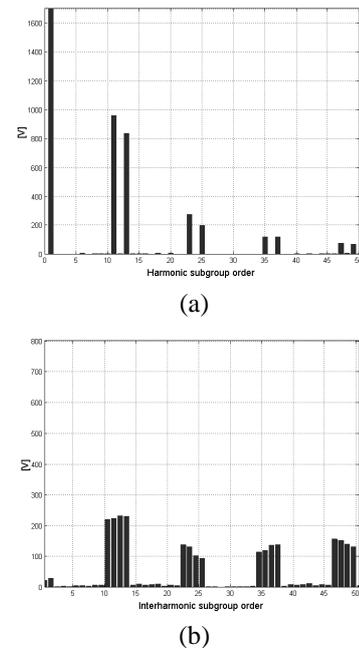


Fig. 5 - IEC harmonic (a) and inter-harmonic (b) subgroup amplitudes of the voltage waveform with separate control systems.

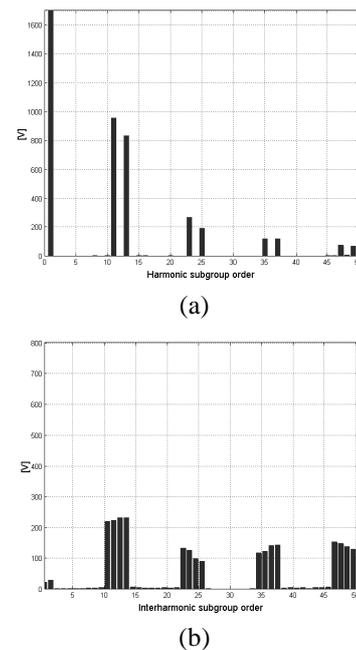


Fig. 6 - IEC harmonic (a) and inter-harmonic (b) subgroup amplitudes of the voltage waveform with one control system.

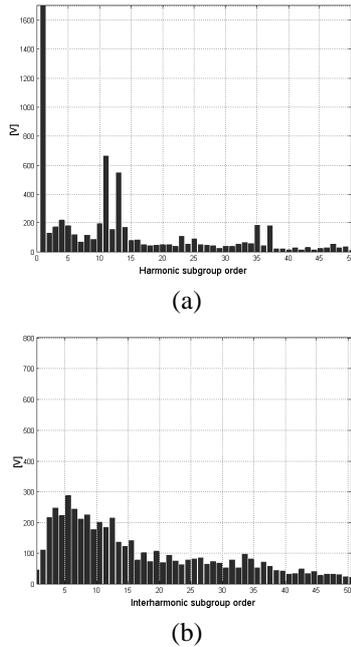


Fig. 7 - IEC harmonic (a) and inter-harmonic (b) subgroup amplitudes of the voltage waveform with incorrect control system parameters.

From the analysis of Figs 5 and 6 it clearly appears that the two different control systems are characterized by very slight differences. As it will be shown in the next, this behaviour holds also in presence of unbalances in the voltage waveforms.

From the analysis of Figs 5 and 7 it clearly appears that the setting of the control system parameters is crucial also with reference to the waveform distortion assessment of the dc arc furnaces. These results fully comply the conclusions of the paper [3]; also with a different representation of the DC arc (in this paper Chua Model based on chaos theory), an incorrect setting of the control system parameters gives unreliable results in the calculation not only of the harmonic subgroups but also of the interharmonic subgroups.

As a further example of waveform distortion assessment, Figs. 8 show the harmonic and interharmonic subgroup amplitudes in presence of a voltage unbalance factor equal to 2%. Only the results obtained with the control system of Fig. 5 has been considered since no significant differences have been detected with the control system of Fig. 6.

The analysis of the Fig. 8 clearly shows that the presence of the voltage unbalances generates new significant harmonic and interharmonic subgroups. It follows that when the DC arc furnaces are fed by a network bus where unbalances can be forecasted, high attention must be paid in waveform distortion evaluation due the strong influence the unbalances have.

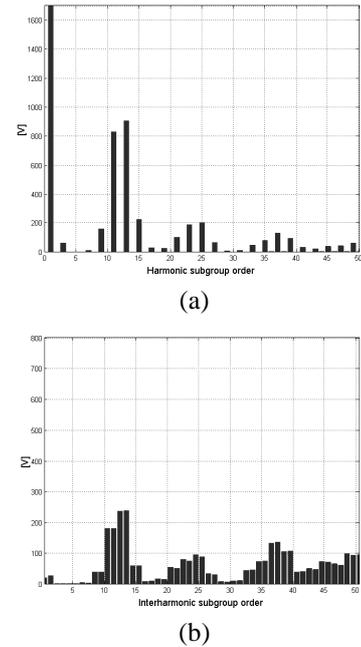


Fig. 8 - IEC harmonic (a) and inter-harmonic (b) subgroup amplitudes of a phase-voltage waveform with 2% of voltage unbalance.

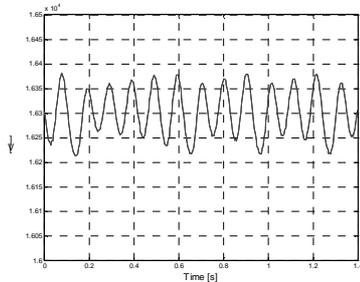
All the results previously shown have been obtained with the use of the FFT. In the relevant literature, other methods have been proposed to capture the time-changes of the spectral components in case of aperiodic signals, as an alternative to FFT. For instance, the Wavelet transform can be also used for this purpose, due to its powerful features of time frequency analysis of nonstationary signals. Recently, in [8] the Prony method was tested for the calculation of several waveform distortion indices in presence of non-stationary signals in power systems; this method is a signal processing technique that approximates a sampled waveform as a linear combination of complex conjugate exponentials. It appears particularly useful when we deal with spectral components with not only amplitude but also frequency variations versus time.

The Prony method can be also useful in assessing the effects of compensation strategies on waveform distortions [8]. For instance, it can be used to calculate the time-variations of the spectral components (fundamental, harmonics and interharmonics) when passive filters are provided in order to reduce the distortions. As well known, the passive filters are one of the most usual compensation strategy used in the AC/DC arc furnace plants.

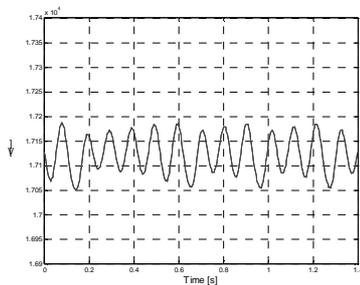
Figs. 9 and 10 show the time variations of the fundamental and 11<sup>th</sup> harmonic without and with passive filters. The passive filters have been chosen on the basis of the Recommendations given by the IEEE Task Force on Interharmonics [9]. In

particular, it was provided two notch filters tuned at 600 Hz and at 1150 Hz; moreover, the unavoidable parallel resonance produced by the notch filter was significantly reduced by a third order high pass filter tuned at 250 Hz [10].

Similar plots can be obtained for the other spectral components. *CTRL*

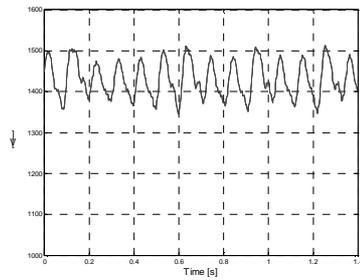


(a)

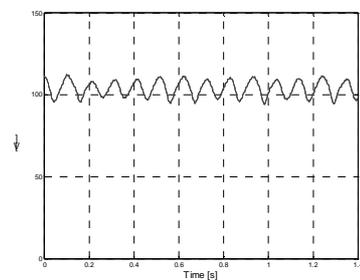


(b)

Fig. 9 - Voltage fundamental versus time obtained with Prony method: (a) without passive filters; (b) with passive filters



(a)

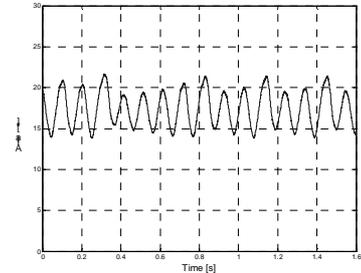


(b)

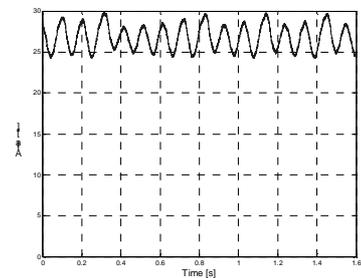
Fig. 10 - 11<sup>th</sup> voltage harmonic versus time obtained with Prony method: (a) without passive filters; (b) with passive filters

The analysis of Figs 9 and 10 clearly reveals that the passive filters guarantee a good

compensation action at harmonic frequencies. Moreover, the control systems act better so that the fluctuations of the spectral components versus time (including the fundamental) reduce. To confirm this consideration, Figs. 11 show the time variations of the converter delay angle (ctrl), once again without (a) and with passive filters (b).



(a)



(b)

Fig. 11 - Converter delay angle versus time: (a) without passive filters; (b) with passive filters

The difference between the maximum and minimum values of the converter delay angle is equal to 7.9° (5.6°) without (with) passive filters.

### Results with Esprit method

## 5. CONCLUSIONS

## 6. REFERENCES

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